## MPQ4436/4436A



45V, 6A, Low I<sub>Q</sub>, Synchronous Step-Down Converter, AEC-Q100 Qualified

#### DESCRIPTION

The MPQ4436/4436A is a frequency programmable, synchronous, step-down switching regulator with integrated internal high-side and low-side power MOSFETs. It provides 6A (or less) of highly efficient output, with current mode control for fast loop response.

The wide 3.3V to 45V input range accommodates a variety of step-down applications in an automotive input environment. A 1.7 $\mu$ A shutdown mode quiescent current allows the part to be used in battery-powered applications.

High power conversion efficiency over a wide load range is achieved by scaling down the switching frequency in light-load conditions to reduce the switching and gate driving losses.

An open-drain power good signal indicates that the output is within 93% to 106% of its nominal voltage.

Frequency foldback helps prevent inductor current runaway during start-up. Thermal shutdown provides reliable, fault-tolerant operation.

High-duty cycle and low dropout mode are provided for the automotive cold crank condition.

The MPQ4436/4436A is available in a QFN-20 (4mmx4mm) package.

#### **FEATURES**

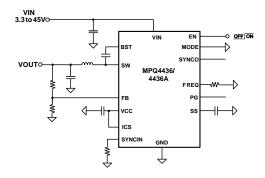
- Wide 3.3V to 45V Operating Voltage Range
- 6A Continuous Output Current
- 1.7μA Low Shutdown Supply Current
- 18µA Sleep Mode Quiescent Current
- Internal  $48m\Omega$  High-Side and  $20m\Omega$  Low-Side MOSFET
- 350kHz to 1000kHz Programmable Switching Frequency for Car Battery Applications
- Synchronize to External Clock
- Multi-Phase Capability
- Out-of-Phase Synchronized Clock Output
- Frequency Spread Spectrum (FSS) Option for Low EMI MPQ4436: Non-FSS version MPQ4436A: FSS version
- Symmetric V<sub>IN</sub> for Low EMI
- Power Good Output
- External Soft Start
- 100ns Minimum On Time
- Selectable Advanced Asynchronous Mode (AAM) or Forced Continuous Conduction Mode (FCCM)
- Low Dropout Mode
- Hiccup Over-Current Protection
- Available in a QFN-20 (4mmx4mm) Package
- Available in a Wettable Flank Package
- Available in AEC-Q100 Grade-1

#### **APPLICATIONS**

- Automotive Infotainment
- Automotive Clusters
- Advanced Driver Assistance Systems
- Industrial Power Systems

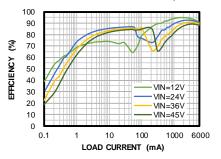
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## **TYPICAL APPLICATION**



#### **Efficiency vs. Load Current**

V<sub>OUT</sub>=3.3V, F<sub>SW</sub>=470kHz, L=3.3μH, AAM



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#### ORDERING INFORMATION

Part Number*	Package Top Marking		MSL Rating**
MPQ4436GRE	QFN-20 (4mmx4mm)	See Below	1
MPQ4436GRE-AEC1	QFN-20 (4mmx4mm)	See Below	1
MPQ4436AGRE	QFN-20 (4mmx4mm)	See Below	1
MPQ4436AGRE-AEC1	QFN-20 (4mmx4mm)	See Below	1

<sup>\*</sup> For Tape & Reel, add suffix -Z (e.g. MPQ4436GRE-AEC1-Z).

#### **TOP MARKING**

MPSYWW

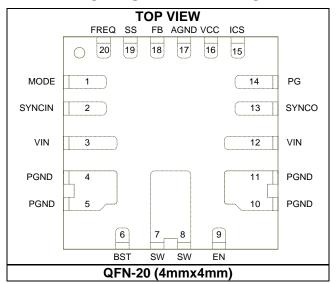
MP4436

LLLLLL

Е

MPS: MPS prefix Y: Year code WW: Week code MP4436: Part number LLLLLL: Lot number E: Wettable flank

## **PACKAGE REFERENCE**



<sup>\*\*</sup>Moisture Sensitivity Level Rating



## **PIN FUNCTIONS**

Pin#	Name	Description
1	MODE	<b>AAM or FCCM select pin.</b> Pull high to put the part in FCCM, and pull low for AAM at light load. Do not leave it floating.
2	SYNCIN	<b>SYNC input.</b> Connect a $51k\Omega$ resistor between SYNCIN and GND. Apply a $350kHz$ to $1000kHz$ clock signal to this pin to synchronize the internal oscillator frequency to the external clock. This pin is also used for multi-phase operation. Connect this pin to GND if not used; do not float it.
3, 12	VIN	<b>Input supply.</b> VIN supplies power to all the internal control circuitry and the power switch connected to SW. It is recommended to place a decoupling capacitor to ground close to VIN to minimize switching spikes.
4, 5, 10, 11	PGND	Power ground.
6	BST	<b>Bootstrap.</b> BST is the positive power supply for the high-side MOSFET driver connected to SW. Connect a bypass capacitor between BST and SW. Check the application section to calculate the size of this capacitor.
7, 8	SW	Switch node. SW is the output of the internal power switch.
9	EN	<b>Enable.</b> Pull this pin below the specified threshold (0.85V) to shut down the chip. Pull it up above the specified threshold (1V) to enable the chip.
13	SYNCO	<b>SYNC output.</b> Output a clock signal 180° out-of-phase with the internal oscillator signal or opposite to the clock signal applied at SYNCIN pin. Leave floating if not used.
14	PG	<b>Power good indicator.</b> The output of PG is an open drain. A pull-up resistor to the power source is needed if PG is used. It goes high if the output voltage is within 93% to 106% of the nominal voltage; and goes low if the output voltage is above 107.5% or below 91% of the nominal voltage.
15	ICS	<b>Current sharing pin.</b> In a multi-phase application, connect the ICS pin of the ICs in parallel to improve the current sharing between different phases. Do not float this pin; connect it to VCC pin or VOUT that is at least 3V in a single-phase application.
16	VCC	<b>Bias supply.</b> This supplies power to the internal control circuit and gate drivers. A decoupling capacitor to ground is required close to this pin. Check the application section to calculate the size of this capacitor.
17	AGND	Analog ground.
18	FB	<b>Feedback input.</b> Connect FB to the center point of the external resistor divider from the output to AGND to set the output voltage. The feedback threshold voltage is 0.815V. Place the resistor divider as close to FB as possible. Avoid placing vias on the FB traces.
19	SS	<b>Soft start input.</b> Place a capacitor from SS to GND to set the soft-start period. The MPQ4436/4436A sources 6µA from SS to the soft-start capacitor at start-up. As the SS voltage rises, the feedback threshold voltage increases to limit inrush current during start-up.
20	FREQ	<b>Switching frequency program.</b> Connect a resistor from this pin to ground to set the switching frequency. Follow the f <sub>SW</sub> vs. R <sub>FREQ</sub> curve in the Typical Performance Characteristics (TPC) section on page 14 to set the frequency.



ABSOLUTE MAXIMUM RATINGS (1)
VIN, EN0.3V to +50V SW0.3V to $V_{\text{IN (MAX)}} + 0.3V$ BST
Lead temperature+260°C Storage temperature65°C to +150°C
ESD Rating Human-body model (HBM) ±2kV Charged-device model (CDM) ±750V
Recommended Operating Conditions
Supply voltage ( $V_{IN}$ )

Thermal Resistance	$oldsymbol{ heta}_{JA}$	$\boldsymbol{\theta}$ JC
QFN-20 (4mmx4mm)		
JESD51-7 <sup>(3)</sup>	44	9°C/W
EVQ4436-R-00A <sup>(4)</sup>	23	2.5°C/W

#### Notes:

- 1) Exceeding these ratings may damage the device.
- 2) The maximum allowable power dissipation is a function of the maximum junction temperature  $T_J$  (MAX), the junction-to-ambient thermal resistance  $\theta_{JA}$ , and the ambient temperature  $T_A$ . The maximum allowable continuous power dissipation at any ambient temperature is calculated by  $P_D$  (MAX) =  $(T_J$  (MAX)  $T_A$ ) /  $\theta_{JA}$ . Exceeding the maximum allowable power dissipation will cause excessive die temperature, and the regulator will go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- 3) Measured on JESD51-7, 4-layer PCB.
- Measured on EVQ4436-R-00A, 9cmx9cm, 4-Layer PCB.



## **ELECTRICAL CHARACTERISTICS**

 $V_{IN} = 12V$ ,  $V_{EN} = 2V$ ,  $T_J = -40$ °C to +125°C, typical values are at  $T_J = 25$ °C, unless otherwise noted.

Parameter	Symbol	Condition	Min	Тур	Max	Units
VIN UVLO rising threshold	IN <sub>UVLO_RISING</sub>		2.8	3.0	3.2	V
VIN UVLO falling threshold	IN <sub>UVLO_FALLING</sub>		2.45	2.65	2.85	V
VIN UVLO hysteresis	INuvlo_HYS			250		mV
VCC voltage	Vcc	I <sub>VCC</sub> = 0A	4.6	4.9	5.2	V
VCC regulation		Ivcc = 30mA		1	4	%
VCC current limit	ILIMIT_VCC	Vcc = 4V	100			mA
VIN quiescent current	ΙQ	FB = 0.85V, no load, (sleep mode)		18	26	μA
		MODE = GND (AAM), switching, no load, $R_{FB\_Up} = 1M\Omega,$ $R_{FB\_Down} = 316k\Omega$		20		μА
VIN quiescent current (switching) (5)	IQ_ACTIVE	MODE = high (FCCM), switching, fsw = 2MHz, no load		40		mA
		MODE = high (FCCM), switching, fsw = 470kHz, no load		9.5		mA
VIN shutdown current	I <sub>SHDN</sub>	EN = 0V		1.7	2.5	μΑ
FB voltage	$V_FB$	$VIN = 3.3V$ to 45V, $T_J = 25$ °C	0.807	0.815	0.823	V
		VIN = 3.3V to 45V	0.799	0.815	0.831	V
FB current	I <sub>FB</sub>	V <sub>FB</sub> = 0.85V	-50	0	50	nA
Switching frequency	f <sub>SW</sub>	$R_{FREQ} = 62k\Omega$	420	470	520	kHz
Minimum on time (5)	ton_min			100		ns
Minimum off time (5)	toff_min			80		ns
SYNCIN voltage rising threshold	VSYNC_RISING		1.8			V
SYNCIN voltage falling threshold	V <sub>SYNC_FALLING</sub>				0.4	V
SYNCIN clock range	fsync	External clock	350		1000	kHz
SYNCO high voltage	Vsynco_high	Isynco = -1mA	3.3	4.5		V
SYNCO low voltage	V <sub>SYNCO_LOW</sub>	Isynco = 1mA			0.4	V
SYNCO phase shift		Tested on SYNCIN		180		Deg
HS current limit	I <sub>LIMIT</sub>	Duty cycle = 30%	10	13	16	Α
LS valley current limit	LIMIT_VALLEY		8	10	12	Α
ZCD current	I <sub>ZCD</sub>	AAM	-0.15	0.1	0.35	Α
LS reverse current limit	I <sub>LIMIT_REVERSE</sub>	FCCM	2	4.5	6.5	Α



## **ELECTRICAL CHARACTERISTICS** (continued)

 $V_{IN} = 12V$ ,  $V_{EN} = 2V$ ,  $T_J = -40$ °C to +125°C, typical values are at  $T_J = 25$ °C, unless otherwise noted.

Parameter	Symbol	Condition	Min	Тур	Max	Units
Switch leakage current	Isw_LKG			0.01	1	μΑ
HS switch on resistance	R <sub>ON_HS</sub>	$V_{BST} - V_{SW} = 5V$		48	80	mΩ
LS switch on resistance	R <sub>ON_LS</sub>	Vcc = 5V		20	40	mΩ
Soft-start current	Iss	Vss = 0V	4	6	8	μA
EN rising threshold	V <sub>EN_RISING</sub>		0.8	1	1.2	V
EN falling threshold	VEN_FALLING		0.65	0.85	1.05	V
EN hysteresis voltage	V <sub>EN_HYS</sub>			180		mV
MODE rising threshold	V <sub>MODE_RISING</sub>		1.8			V
MODE falling threshold	V <sub>MODE_FALLING</sub>				0.4	V
DC riging throughold (\(\lambda_{}\)/\(\lambda_{}\)	DC	V <sub>FB</sub> rising	88.5%	93%	97.5%	
PG rising threshold (V <sub>FB</sub> / V <sub>REF</sub> )	PGRISING	V <sub>FB</sub> falling	101.5%	106%	110.5%	V <sub>REF</sub>
DC falling throughold ()/ /)/	PGFALLING	V <sub>FB</sub> falling	86.5%	91%	95.5%	
PG falling threshold (V <sub>FB</sub> / V <sub>REF</sub> )	FGFALLING	V <sub>FB</sub> rising	103%	107.5%	112%	
PG output voltage low	$V_{PG\_LOW}$	Isink = 1mA		0.1	0.3	V
PG rising delay	tpg_r_delay			30		μs
PG falling delay	tpg_f_delay			30		μs
Thermal shutdown (5)	tsp			170		°C
Thermal shutdown hysteresis (5)	t <sub>SD_HYS</sub>			20		°C

#### Note:

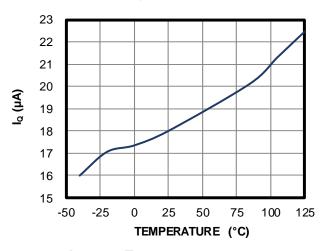
<sup>5)</sup> Derived from bench characterization, not tested in production.



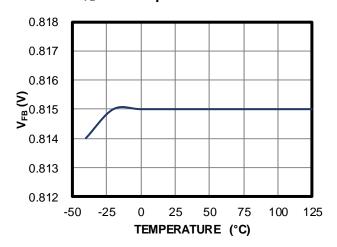
## TYPICAL CHARACTERISTICS

 $V_{IN} = 12V$ ,  $T_J = -40$ °C to +125°C, unless otherwise noted.

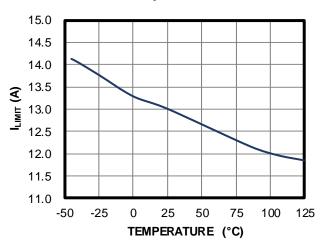




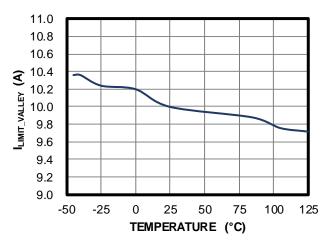
V<sub>FB</sub> vs. Temperature



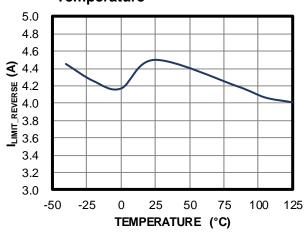
ILIMIT vs. Temperature



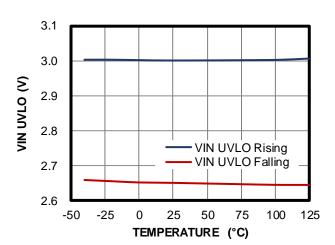
Valley Current Limit vs. Temperature



Reverse Current Limit vs. **Temperature** 



**VIN UVLO Threshold vs. Temperature** 

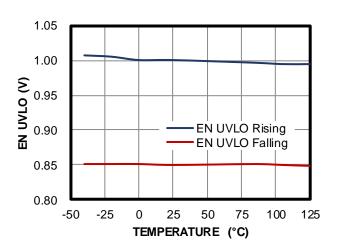




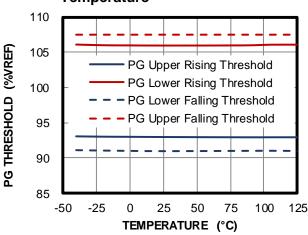
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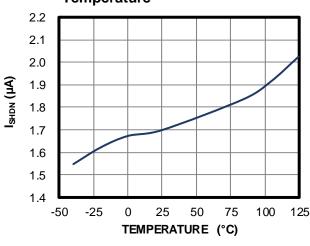
#### **EN UVLO Threshold vs. Temperature**



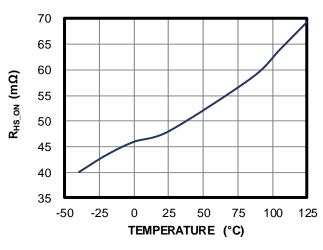
#### PG Rising/Falling Threshold vs. **Temperature**



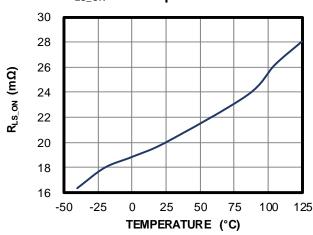
VIN Shutdown Current vs. **Temperature** 



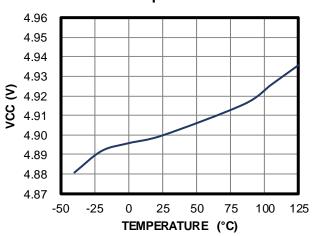
R<sub>HS ON</sub> vs. Temperature



R<sub>LS</sub> ON vs. Temperature



VCC vs. Temperature



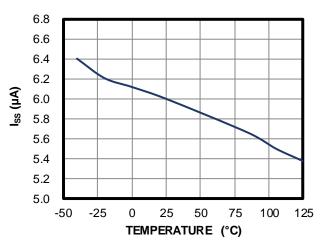
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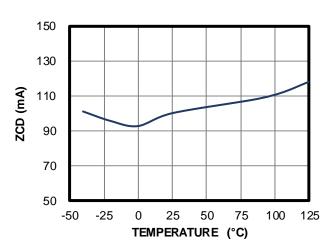
## TYPICAL CHARACTERISTICS (continued)

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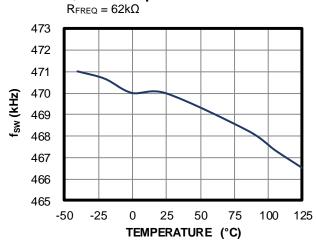
#### Soft-Start Current vs. Temperature



**ZCD vs. Temperature** 

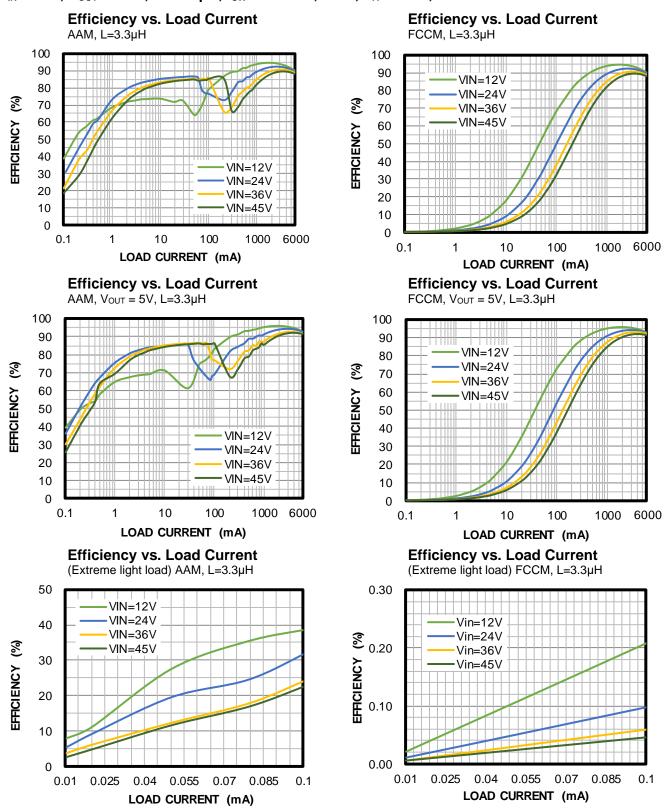


#### fsw vs. Temperature

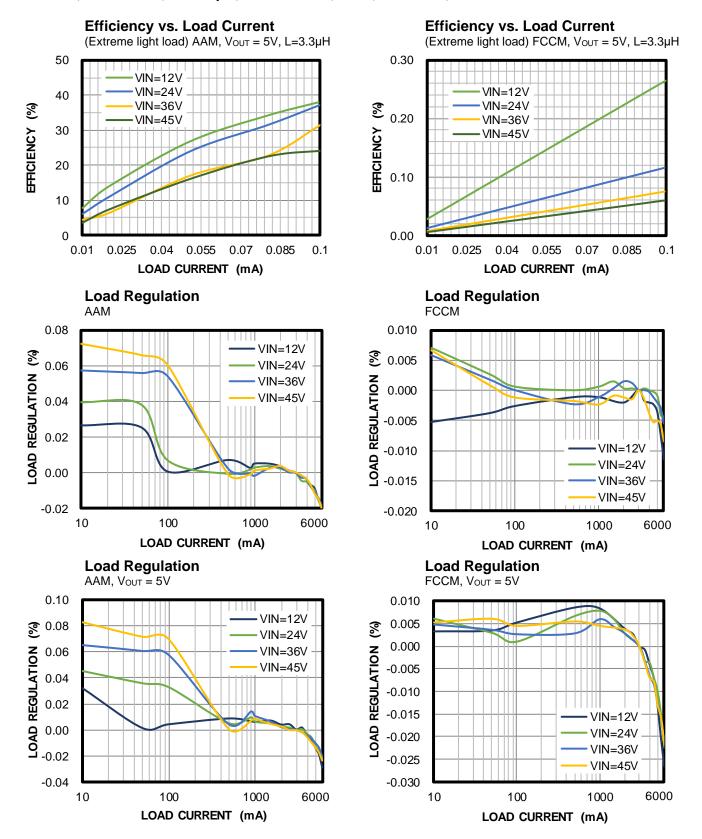




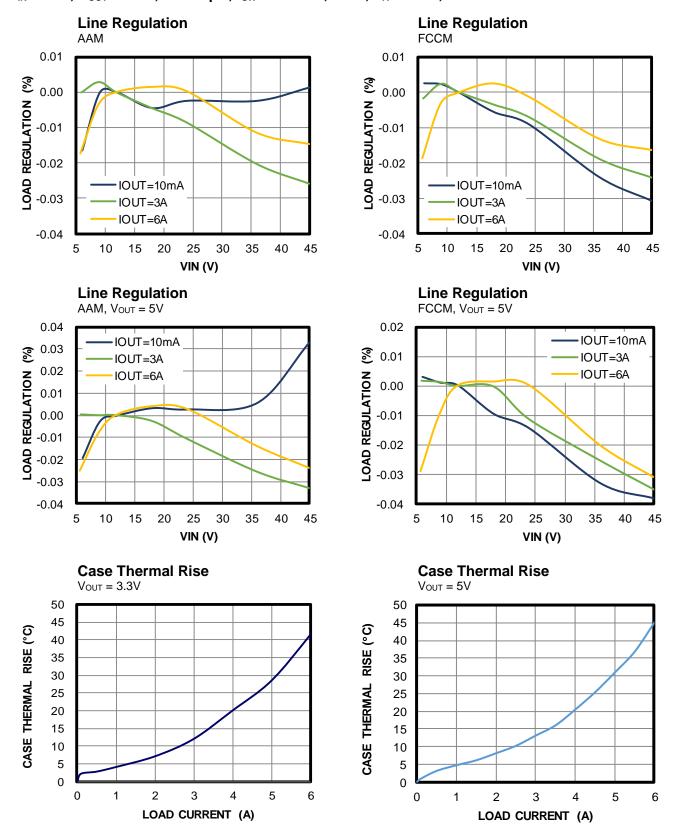
#### TYPICAL PERFORMANCE CHARACTERISTICS



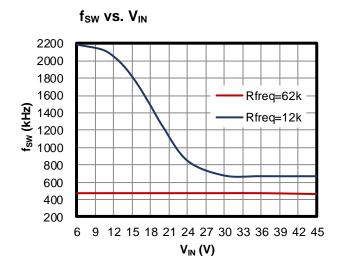


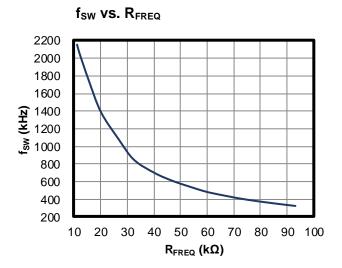


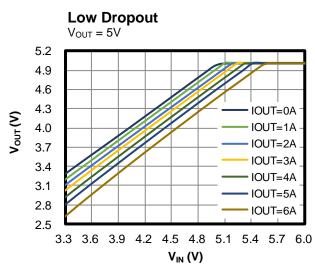










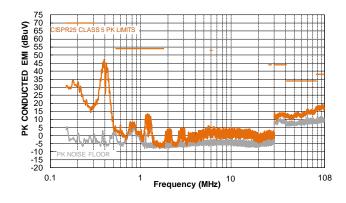


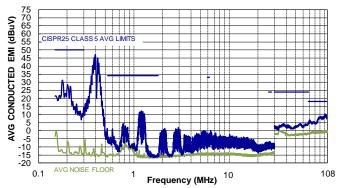


 $V_{IN} = 12V$ ,  $V_{OUT} = 5V$ ,  $I_{OUT} = 6A$ ,  $L = 4.7\mu H$ ,  $f_{SW} = 410 kHz$ ,  $T_A = 25$ °C, with FSS (MPQ4436A only), unless otherwise note. (6)

#### **CISPR25 Class 5 Peak Conducted Emissions** 150kHz to 108MHz

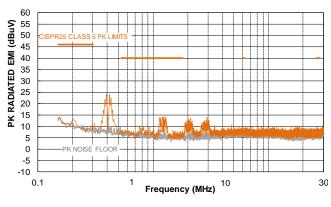
**CISPR25 Class 5 Average Conducted Emissions** 150kHz to 108MHz

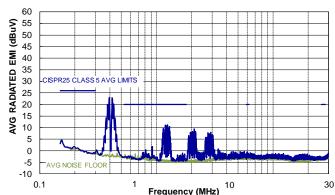




#### **CISPR25 Class 5 Peak Radiated Emissions** 150kHz to 30MHz

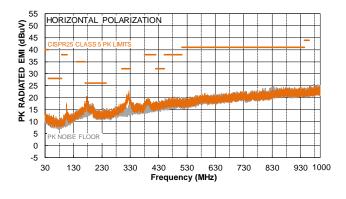
**CISPR25 Class 5 Average Radiated Emissions** 150kHz to 30MHz

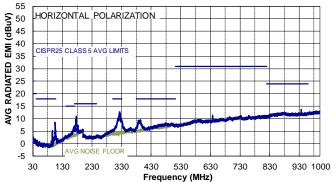




#### **CISPR25 Class 5 Peak Radiated Horizontal** 30MHz to 1GHz

### **CISPR25 Class 5 Average Radiated Horizontal** 30MHz to 1GHz





15 MPQ4436/4436A Rev. 1.2 MonolithicPower.com

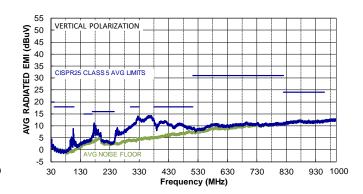


 $V_{IN}$  = 12V,  $V_{OUT}$  = 5V,  $I_{OUT}$  = 6A, L = 4.7 $\mu$ H,  $f_{SW}$  = 410kHz,  $T_A$  = 25°C, with FSS (MPQ4436A only), unless otherwise noted.  $^{(6)}$ 

# CISPR25 Class 5 Peak Radiated Emissions Vertical, 30MHz to 1GHz

#### 

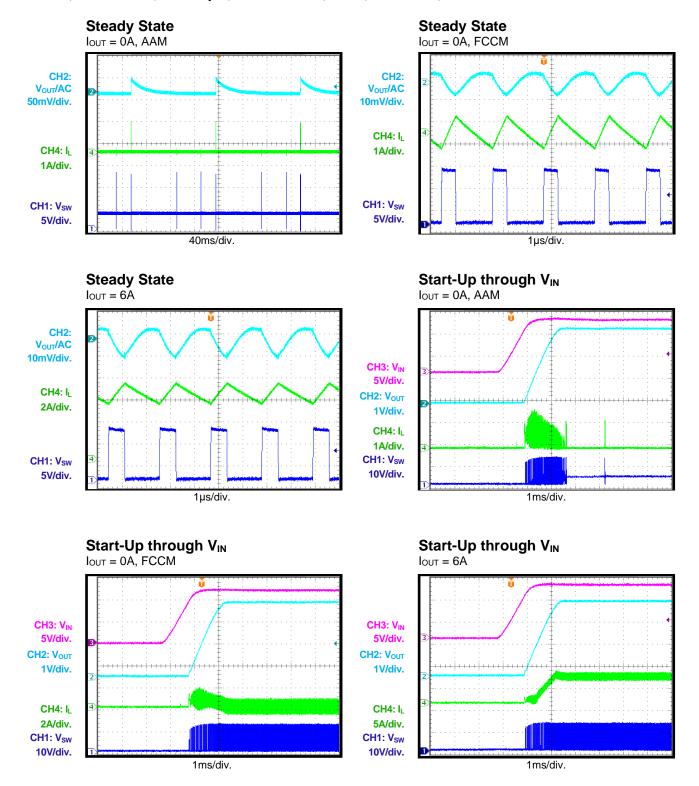
# CISPR25 Class 5 Average Radiated Emissions Vertical, 30MHz to 1GHz



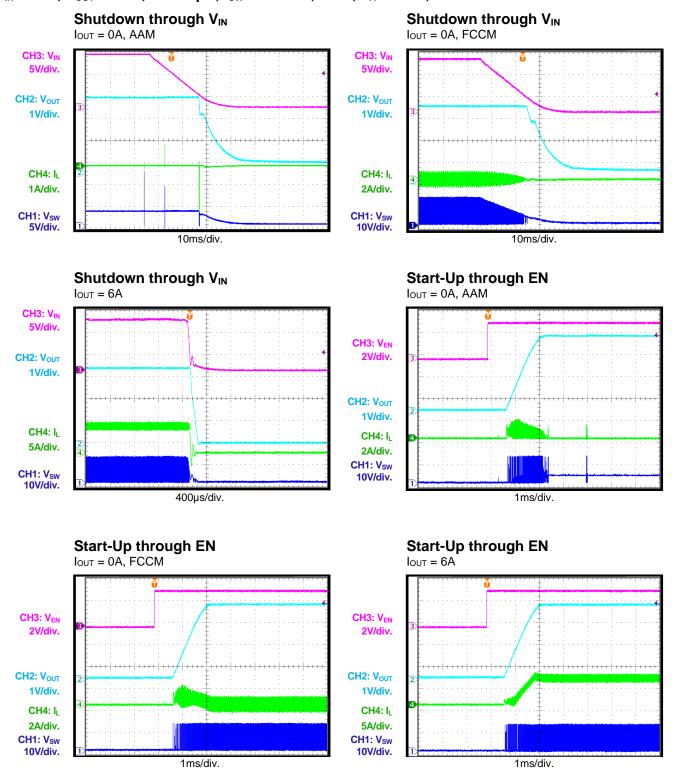
#### Note:

6) The EMC test results are based on the application circuit with EMI filters (see Figure 13).

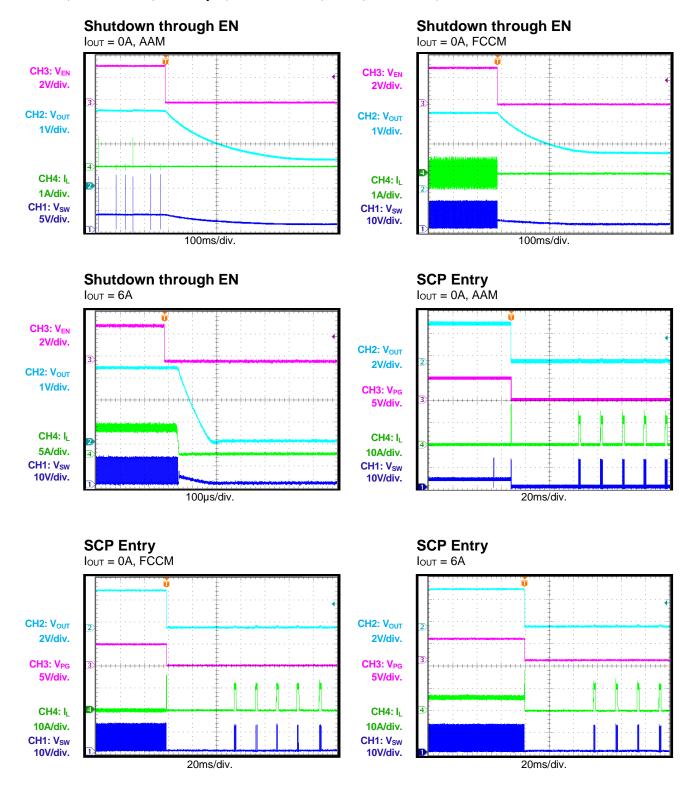




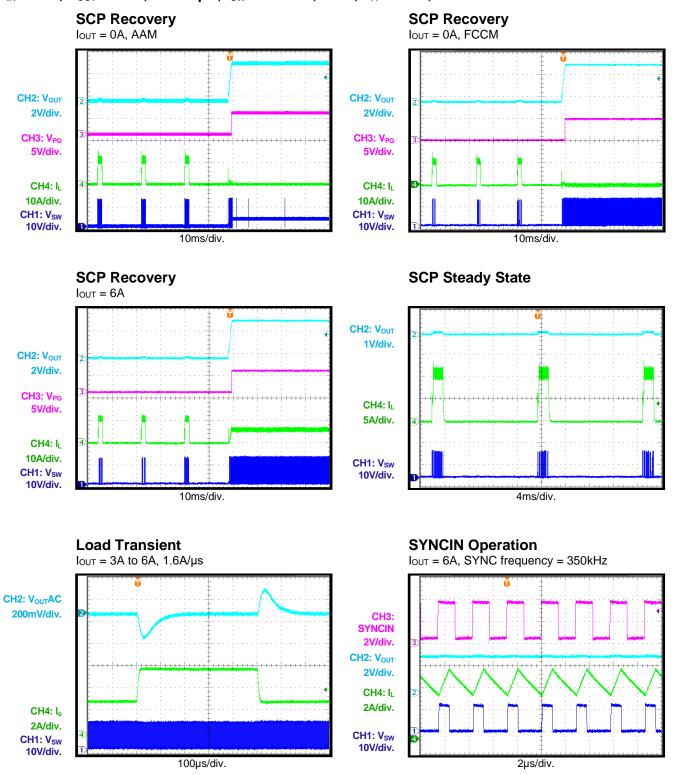




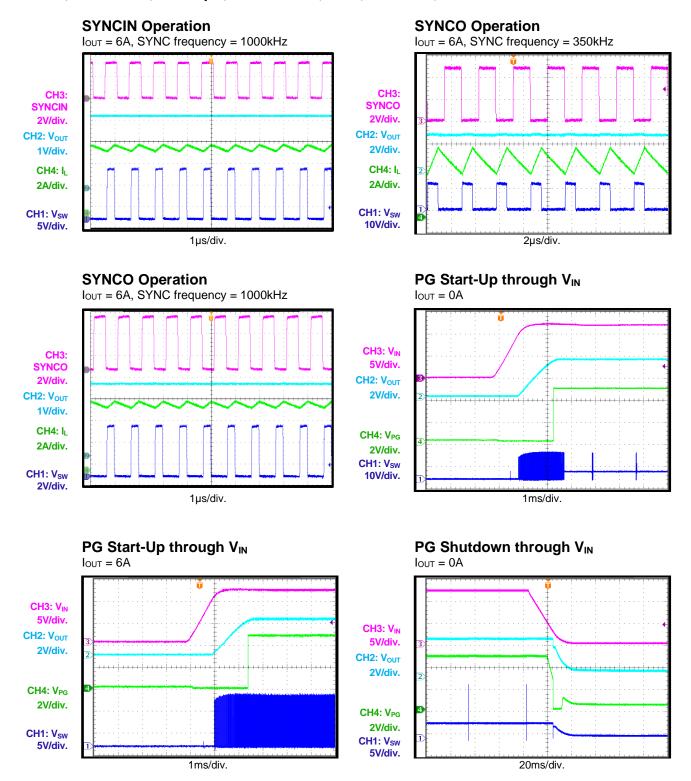




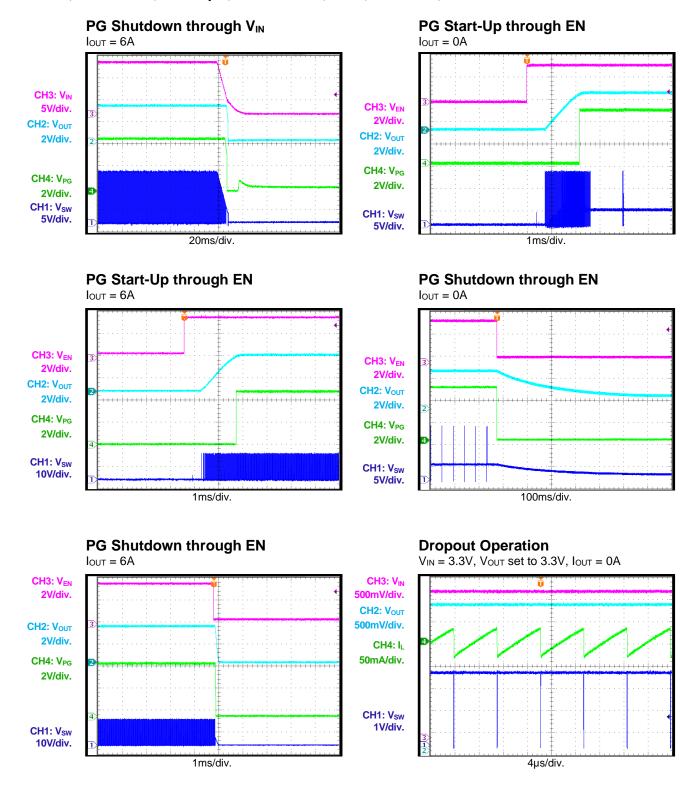




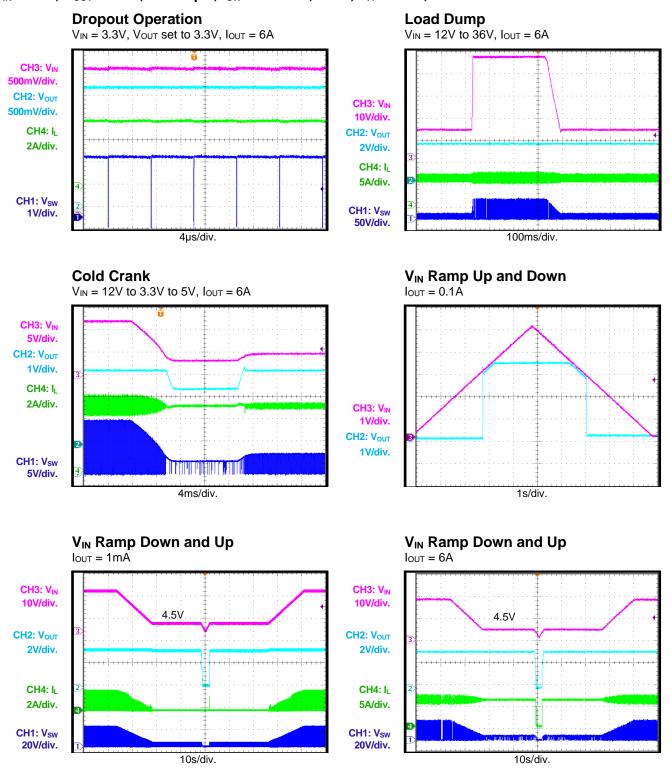










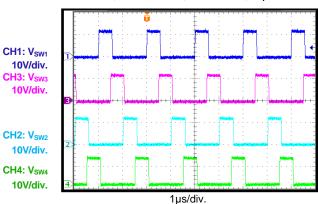




 $V_{IN}$  = 12V,  $V_{OUT}$  = 3.3V, L = 4.7 $\mu$ H,  $f_{SW}$  = 470kHz, AAM,  $T_A$  = 25°C, unless otherwise noted.

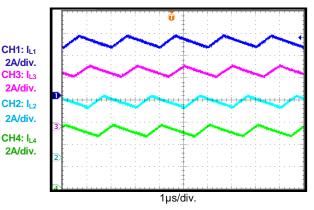


Steady State  $V_{IN} = 12V$ ,  $V_{OUT} = 3.3V$ ,  $I_{OUT} = 20A$ , 4-phase



#### **Steady State**

 $V_{IN} = 12V$ ,  $V_{OUT} = 3.3V$ ,  $I_{OUT} = 20A$ , 4-phase



## **FUNCTION BLOCK DIAGRAM**

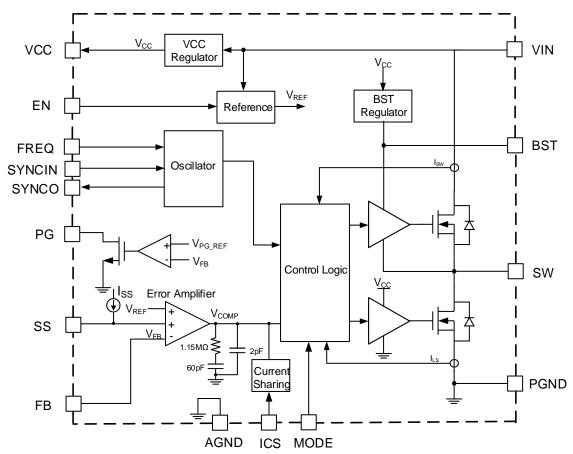


Figure 1: Functional Block Diagram

## **Timing Sequence**

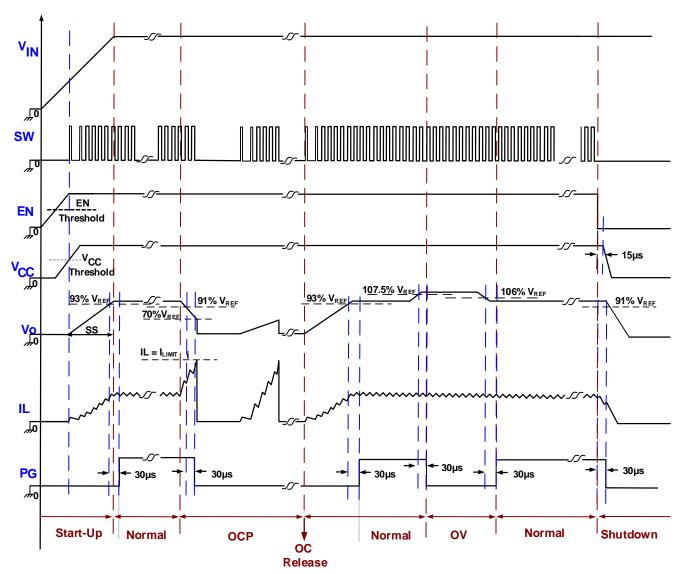


Figure 2: Timing Sequence



#### **OPERATION**

The MPQ4436/4436A is a synchronous, step-down switching regulator with integrated internal high-side and low-side power MOSFETs. It provides 6A of highly efficient output with current mode control.

It features a wide input voltage range, programmable switching frequency, external soft start, and precision current limiting. Its very low operational quiescent current makes it ideal for battery-powered applications.

#### **PWM Control**

At moderate to high output current, the MPQ4436/4436A operates in a fixed-frequency, peak current control mode to regulate the output voltage. A PWM cycle is initiated by the internal clock. At the rise edge of the clock, the high-side MOSFET (HS-FET) turns on and remains on until its current reaches the value set by the internal COMP voltage ( $V_{\text{COMP}}$ ). Once the HS-FET is on, it remains on for at least 100ns.

When the high-side power switch is off, the lowside MOSFET (LS-FET) turns on immediately and remains on until the next cycle starts. Once the LS-FET is on, it remains on for at least 80ns before next cycle starts.

If, in one PWM period, the current in the HS-FET does not reach the COMP-set current value, the HS-FET remains on, saving a turn-off operation. The HS-FET is forced off if the on time lasts about 10µs, even though COMP is not reached.

#### **Light-Load Operation**

11/8/2021

In a light-load condition, the MPQ4436/4436A can work at two different operation modes by setting the MODE pin to one of two different statuses.

The MPQ4436/4436A works in forced CCM when the CCM pin is pulled above 1.8V. The part works with fixed frequency from no load to full load at this mode. The advantage of CCM is the controllable frequency and lower output ripple at light load.

The MPQ4436/4436A works in asynchronous advanced mode (AAM) when the MODE pin is pulled below 0.4V. AAM is meant to optimize the efficiency during light-load and no-load conditions.

When AAM is enabled, the MPQ4436/4436A first enters non-synchronous operation as long as the inductor current approaches zero at light load. If the load is further decreased or there is no load that makes  $V_{\text{COMP}}$  decrease to the set value, the MPQ4436/4436A enters AAM. In AAM, the internal clock is reset every time  $V_{\text{COMP}}$  crosses over the set value. The crossover time is taken as the benchmark of the next clock. When the load increases and  $V_{\text{COMP}}$  exceeds the set value, the operation mode is DCM or CCM, which has a constant switching frequency (see Figure 3).

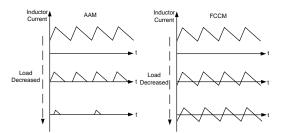


Figure 3: AAM and FCCM

#### **Error Amplifier**

The error amplifier compares the FB pin voltage with the internal reference (0.815V) and outputs a current proportional to the difference between the two. This output current is then used to charge the compensation network to form  $V_{\text{COMP}}$ , which is used to control the power MOSFET current.

During operation, the minimum  $V_{\text{COMP}}$  is clamped to 0.9V, and its maximum is clamped to 2.0V. COMP is internally pulled down to GND in shutdown mode.

#### **Internal Regulator VCC**

Most of the internal circuitry is powered on by the internal 4.9V VCC regulator. This regulator takes VIN as the input and operates in the full VIN range. When VIN is greater than 4.9V, VCC is in full regulation. When VIN is below this point, the output VCC degrades.

#### **Bootstrap Charging**

The bootstrap capacitor is charged and regulated to about 5V by the dedicated internal bootstrap regulator. When the voltage between a BST and SW nodes is lower than its regulation, a PMOS pass transistor connected from VCC to BST turns on to charge the bootstrap capacitor. External

circuitry should provide enough voltage headroom to facilitate the charging.

When the HS-FET is on, BST is above VCC, so the bootstrap capacitor cannot be charged.

In higher duty cycle operation conditions, the time period available to the bootstrap charging is less, so the bootstrap capacitor may not be charged sufficiently. If the external circuit has not had sufficient voltage and time to charge the bootstrap capacitor, extra external circuitry can be used to ensure the bootstrap voltage is in the normal operation range.

#### **Low Dropout Operation and BST Refresh**

To improve dropout, the MPQ4436/4436A is designed to operate at close to 100% duty cycle as long as the BST-to-SW voltage is greater than 2.5V. When the voltage from BST to SW drops below 2.5V, the HS-FET turns off using a UVLO circuit, which allows the LS-FET to conduct and refresh the charge on the BST capacitor. In DCM mode or PSM mode, the LS-FET is forced on to refresh the BST voltage.

Since the supply current sourced from the BST capacitor is low, the HS-FET remains on for more switching cycles than are required to refresh the capacitor. Therefore, the effective duty cycle of the switching regulator is high.

The effective duty cycle during dropout of the regulator is mainly influenced by the voltage drops across the power MOSFET, inductor resistance, the low-side diode, and PCB resistance.

#### **Enable Control**

EN is a digital control pin that turns the regulator on and off (see Figure 4). It offers two main features:

#### 1) Enabled by external logic H/L signal

When EN is pulled below the falling voltage threshold (0.85V), the chip is put into the lowest shutdown current mode. Forcing this pin above the EN rising threshold voltage (1V) turns on the part.

# 2) Programmable VIN under-voltage lockout (UVLO)

With high enough  $V_{\text{IN}}$ , the chip can be enabled and disabled by the EN pin. With the internal current source, this circuit can generate a programmable  $V_{\text{IN}}$  UVLO and hysteresis.

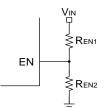


Figure 4: Enable Divider Circuit

#### **Frequency Programmable and Foldback**

The MPQ4436/4436A oscillating frequency is programmed either by an external resistor ( $R_{FREQ}$ ) from the FREQ pin to ground, or by a logic level SYNC signal.

To get an expected switching frequency (f<sub>SW</sub>), select the R<sub>FREQ</sub> value following the f<sub>SW</sub> vs. R<sub>FREQ</sub> curve in the Typical Performance Characteristics (TPC) section on page 14. Note that f<sub>SW</sub> will fold back at high V<sub>IN</sub> when set at high values to avoid triggering the minimum on time and the output going out of regulation. The f<sub>SW</sub> vs. V<sub>IN</sub> curve in the TPC section shows an example when R<sub>FREQ</sub> is  $12k\Omega$ . The corresponding  $f_{SW}$  is about 2.1MHz at VIN = 12V, and decreases to be below 1.5MHz when VIN is above 18V. Thus the switching frequency drops into the AM band (<1.8MHz), which should be avoided for car battery applications considering EMI compliance. So the recommended f<sub>SW</sub> of the MPQ4436/4436A for car battery applications is 350kHz to 1000kHz. Higher frequencies may still be supported for the applications that do not have critical limits on the switching frequency or have relatively low, stable input voltages.

#### Frequency Spread Spectrum (MPQ4436A Only)

MPQ4436A uses a 12kHz modulation frequency with at most a 128-step triangular profile to spread the internal oscillator frequency over a 20% (±10%) window. The steps are fixed and independent of the setting oscillator frequency to optimize the frequency spread spectrum (FSS) performance (see Figure 5).

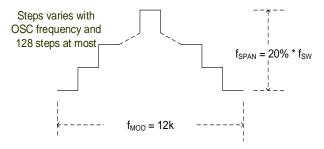


Figure 5: Spread Spectrum Scheme



Side bands are created by modulating the switching frequency with the triangle modulation waveform. The emission power fundamental switching frequency and its harmonics is distributed into smaller pieces. Thus, the peak EMI noise is reduced significantly.

#### **Soft Start**

Soft start is implemented to prevent the converter output voltage from overshooting during start-up.

When the soft-start period starts, an internal current source begins charging the external softstart capacitor. When the soft-start voltage (SS) is below the internal reference (REF), SS overrides REF so the error amplifier uses SS as the reference. When SS exceeds REF, REF regains control. C<sub>SS</sub> can be calculated with Equation (1):

$$C_{SS}(nF) = \frac{t_{SS}(ms) \times I_{SS}(\mu A)}{V_{REF}(V)} = 6.25 \times t_{SS}(ms)$$
 (1)

The SS pins can be used for tracking and sequencing.

#### **Pre-Bias Start-Up**

For the MPQ4436/4436A, if FB > SS - 150mV at start-up (which means the output has a pre-bias voltage), neither the HS-FET nor LS-FET are turned on until SS exceeds FB.

#### **Thermal Shutdown**

11/8/2021

Thermal shutdown is implemented to prevent the chip from thermally running away. When the silicon die temperature exceeds its upper threshold, it shuts down the power MOSFETs. When the temperature falls below its lower threshold, the chip is enabled again.

#### **Current Comparator and Current Limit**

The power MOSFET current is accurately sensed via a current-sense MOSFET. It is then fed to the high speed current comparator for current mode control. The current comparator takes this sensed current as one of its inputs.

When the HS-FET turns on, the comparator is blanked until the end of the turn-on transition to dodge the noise. Then, the comparator compares the power switch current with V<sub>COMP</sub>. When the sensed current exceeds  $V_{COMP}$ , the comparator outputs low to turn off the HS-FET. The maximum current of the internal power MOSFET is internally limited cycle by cycle.

#### **Hiccup Protection**

When the output is shorted to ground, causing the output voltage to drop below 70% of its nominal output, the IC is shut down momentarily and begins discharging the soft-start capacitor. It restarts with a full soft start when the soft-start capacitor is fully discharged. This hiccup process is repeated until the fault is removed.

#### Start-Up and Shutdown

If both VIN and EN exceed their respective thresholds, the chip starts. The reference block starts first, generating a stable reference voltage and currents, and then the internal regulator is enabled. The regulator provides a stable supply for the remaining circuitries.

While the internal supply rail is up, an internal timer holds the power MOSFET off for about 50µs to blank the start-up glitches. When the soft-start block is enabled, it first holds its SS output low to ensure the remaining circuitries are ready, then slowly ramps up.

Three events shut down the chip: EN low, VIN low, and thermal shutdown. In the shutdown procedure, the signaling path is blocked first to avoid any fault triggering. V<sub>COMP</sub> and the internal supply rail are then pulled down. The floating driver is not subject to this shutdown command, but its charging path is disabled.

#### **Power Good Output**

The MPQ4436/4436A includes an open-drain power good output that indicates the output. A pull-up resistor to power source is needed if PG is used. It goes high if the output voltage is within 93% to 106% of the nominal voltage, and goes low when the output voltage is above 107.5% or below 91% of the nominal voltage.

#### SYNCIN and SYNCO

The switching frequency can be synced to the rising edge of the clock signal applied at SYNCIN. The recommended SYNCIN frequency range is 350kHz to 1000kHz. Ensure that the off time of SYNCIN is shorter than the internal oscillator period, otherwise the internal clock may turn on the HS-FET before the rising edge of SYNCIN. There is no other special limit on the pulse width of SYNCIN, but note that there is always parasitic capacitance of the pad there. If the



pulse width is too short, a clear rising and falling edge may not be seen due to the parasitic capacitance. A pulse longer than 100ns is recommended in application.

When applying SYNCIN in AAM, Drive SYNCIN below its specified threshold (0.4V) or leaving SYNCIN floating before MPQ4436/4436A starting up to enter AAM. And then adding external SYNCIN clock.

The SYNCO pin provides a default 180° phaseshifted clock to the internal oscillator when there is no SYNCIN signal or a clock signal reverse to SYNCIN if an external clock signal is applied at SYNCIN (see Figure 6). This makes enabling a dual-phase, interleaved configuration easy (see Figure 7).

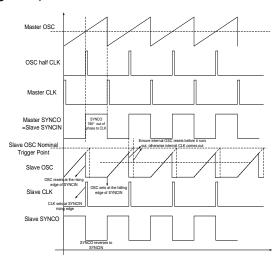


Figure 6: SYNCIN & SYNCO Scheme

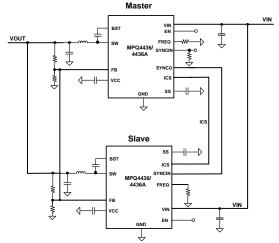
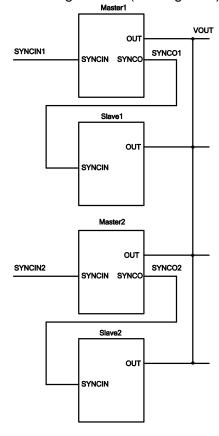


Figure 7: Dual-Phase Configuration

For multi-phase applications, VOUT, FB, and ICS of the chips in parallel need to be connected

together. SYNCO of the master is connected to the SYNCIN pin of the slave for phase interleaved configurations (see Figure 8).



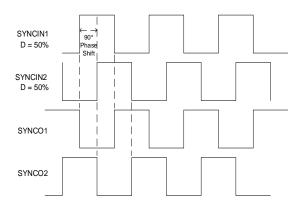


Figure 8: Four-Phase Configuration

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#### APPLICATION INFORMATION

#### **Setting the BST Capacitor**

If using the MPQ4436/4436A in CCM only, use a BST capacitor of  $0.2\mu F$  or greater nominal. If using AAM mode, the external BST capacitor should be greater than  $0.2\mu F$ . Alternately, choose the BST capacitor with Equation (2) and Equation (3):

$$C_{\text{BST}}\left(\mu F\right) \ge \frac{75 \times C_{\text{OUT}}\left(\mu F\right) \times 10^{-3}}{I_{\text{MIN}}\left(\mu A\right)} \tag{2}$$

$$C_{\text{BST}}\left(\mu F\right) \ge \frac{80}{I_{\text{MIN}}\left(\mu A\right) \times L\left(\mu H\right)} \tag{3}$$

If the calculated  $C_{\text{BST}}$  is greater than  $6.8\mu F$ , contact a field applications engineer to verify the design.

#### **Setting the VCC Capacitor**

The VCC capacitor should be 10 times larger than the boost capacitor, and at least  $4.7\mu F$  nominal. A VCC capacitor greater than  $68\mu F$  nominal is not recommended.

#### **Setting the Output Voltage**

The external resistor divider connected to FB sets the output voltage (see Figure 9).

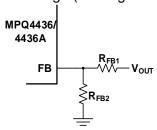


Figure 9: Feedback Network

Choose  $R_{FB1}$  to be about  $40k\Omega$ . Then calculate  $R_{FB2}$  with Equation (4):

$$R_{FB2} \ge \frac{R_{FB1}}{\frac{V_{OUT}}{0.8V} - 1}$$
 (4)

Table 1 lists the recommended feedback resistor values for common output voltages.

**Table 1: Resistor Selection for Output Voltages** 

V <sub>OUT</sub> (V)	R <sub>FB1</sub> (kΩ)	R <sub>FB2</sub> (kΩ)
3.3	100 (1%)	31.6 (1%)
5	100 (1%)	19.1 (1%)

#### **Selecting the Input Capacitor**

The step-down converter has a discontinuous input current, and requires a capacitor to supply AC current to the converter while maintaining the DC input voltage. For the best performance, use low-ESR capacitors. Ceramic capacitors with X5R or X7R dielectrics are highly recommended because of their low ESR and small temperature coefficients.

For most applications, use a 4.7µF to 10µF capacitor. It is strongly recommended to use another, lower value capacitor (e.g. 0.1µF) with a small package size (0603) to absorb high-frequency switching noise. Place the smaller capacitor as close to VIN and GND as possible.

Since  $C_{IN}$  absorbs the input switching current, it requires an adequate ripple current rating. The RMS current in the input capacitor can be estimated with Equation (5):

$$I_{CIN} = I_{LOAD} \times \sqrt{\frac{V_{OUT}}{V_{IN}} \times (1 - \frac{V_{OUT}}{V_{IN}})}$$
 (5)

The worst-case condition occurs at  $VIN = 2V_{OUT}$ , calculated with Equation (6):

$$I_{CIN} = \frac{I_{LOAD}}{2} \tag{6}$$

For simplification, choose an input capacitor with an RMS current rating greater than half of the maximum load current.

The input capacitor can be electrolytic, tantalum, or ceramic. When using electrolytic or tantalum capacitors, add a small, high-quality ceramic capacitor (e.g.  $0.1\mu F$ ) as close to the IC as possible. When using ceramic capacitors, ensure that they have enough capacitance to provide a sufficient charge to prevent excessive voltage ripple at the input. The input voltage ripple caused by the capacitance can be estimated with Equation (7):

$$\Delta V_{IN} = \frac{I_{LOAD}}{f_{SW} \times C_{IN}} \times \frac{V_{OUT}}{V_{IN}} \times (1 - \frac{V_{OUT}}{V_{IN}})$$
 (7)

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#### **Selecting the Output Capacitor**

The output capacitor maintains the DC output voltage. Use ceramic, tantalum, or low-ESR electrolytic capacitors. For best results, use low-ESR capacitors to keep the output voltage ripple low. The output voltage ripple can be estimated with Equation (8):

$$\Delta V_{\text{OUT}} = \frac{V_{\text{OUT}}}{f_{\text{SW}} \times L} \cdot (1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}}) \cdot (R_{\text{ESR}} + \frac{1}{8f_{\text{SW}} \times C_{\text{OUT}}})$$
(8)

Where L is the inductor value, and  $R_{\text{ESR}}$  is the equivalent series resistance (ESR) value of the output capacitor.

For ceramic capacitors, the capacitance dominates the impedance at the switching frequency and causes the majority of the output voltage ripple. For simplification, the output voltage ripple can be estimated with Equation (9):

$$\Delta V_{\text{OUT}} = \frac{V_{\text{OUT}}}{8 \times f_{\text{SW}}^2 \times L \times C_{\text{OUT}}} \times (1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}}) \quad (9)$$

For tantalum or electrolytic capacitors, the ESR dominates the impedance at the switching frequency. For simplification, the output ripple can be estimated with Equation (10):

$$\Delta V_{OUT} = \frac{V_{OUT}}{f_{SW} \times L} \times (1 - \frac{V_{OUT}}{V_{IN}}) \times R_{ESR}$$
 (10)

The characteristics of the output capacitor also affect the stability of the regulation system. The MPQ4436/4436A can be optimized for a wide range of capacitance and ESR values.

#### Selecting the Inductor

A 1µH to 10µH inductor with a DC current rating at least 25% higher than the maximum load current is recommended for most applications. For higher efficiency, choose an inductor with a lower DC resistance. A larger-value inductor results in less ripple current and a lower output ripple voltage, but also has a larger physical size, higher series resistance, and lower saturation current. A good rule for determining the inductor value is to allow the inductor ripple current to be approximately 30% of the maximum load current. The inductance value can be calculated with Equation (11):

$$L = \frac{V_{OUT}}{f_{SW} \times \Delta I_{I}} \times (1 - \frac{V_{OUT}}{V_{IN}})$$
 (11)

Where  $\Delta I_{\perp}$  is the peak-to-peak inductor ripple current.

Choose the inductor ripple current to be approximately 30% of the maximum load current. The maximum inductor peak current can be calculated with Equation (12):

$$I_{LP} = I_{LOAD} + \frac{V_{OUT}}{2f_{SW} \times L} \times (1 - \frac{V_{OUT}}{V_{IN}})$$
 (12)

#### **VIN UVLO Setting**

The MPQ4436/4436A has an internal, fixed under-voltage lockout (UVLO) threshold. The rising threshold is 3V, while the falling threshold is about 2.65V. For applications that need a higher UVLO point, an external resistor divider between VIN and EN can be used to achieve a higher equivalent UVLO threshold (see Figure 10).

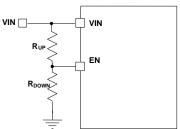


Figure 10: Adjustable UVLO Using EN Divider

The UVLO threshold can be calculated with Equation (13) and Equation (14):

$$INUV_{RISING} = (1 + \frac{R_{UP}}{R_{DOWN}}) \times V_{EN\_RISING}$$
 (13)

$$INUV_{FALLING} = \left(1 + \frac{R_{UP}}{R_{DOWN}}\right) \times V_{EN\_FALLING}$$
 (14)

Where V<sub>EN RISING</sub> is 1V, and V<sub>EN FALLING</sub> is 0.85V.



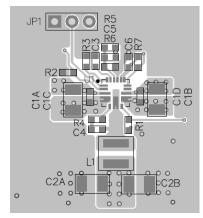
#### PCB Layout Guidelines (7)

Efficient PCB layout, especially for input capacitor placement, is critical for stable 4-layer layout is strongly operation. A recommended to achieve better thermal performance. For best results, refer to Figure 11 and follow the guidelines below:

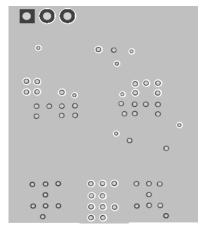
- Place symmetric input capacitors as close to VIN and GND as possible.
- Use a large ground plane to connect directly to PGND.
- 3. Add vias near PGND if the bottom layer is a ground plane.
- 4. Ensure that the high-current paths at GND and VIN have short, direct, and wide traces.
- Place the ceramic input capacitor, especially the small package size (0603) input bypass capacitor, as close to VIN and PGND as possible to minimize high-frequency noise.
- 6. Keep the connection of the input capacitor and VIN as short and wide as possible.
- 7. Place the VCC capacitor as close to VCC and GND as possible.
- 8. Route SW and BST away from sensitive analog areas, such as FB.
- 9. Place the feedback resistors close to the chip to ensure the trace that connects to FB is as short as possible.
- 10. Use multiple vias to connect the power planes to the internal layers.

#### Note:

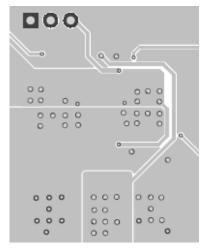
7) The recommended PCB layout is based on Figure 12.



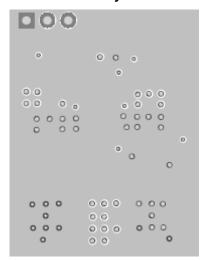
Top Layer



**Inner Layer 1** 



**Inner Layer 2** 



**Bottom Layer** Figure 11: Recommended PCB Layout



## TYPICAL APPLICATION

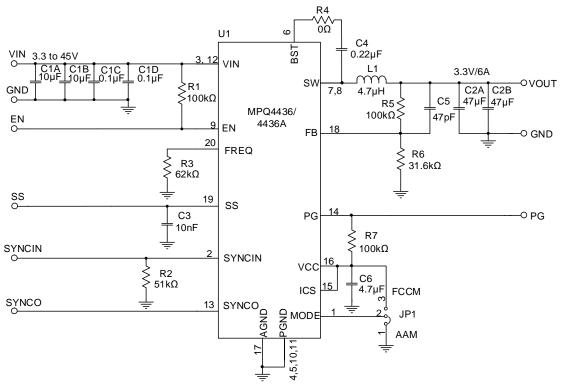


Figure 12: Single-Phase, Vout = 3.3V, fsw = 470kHz

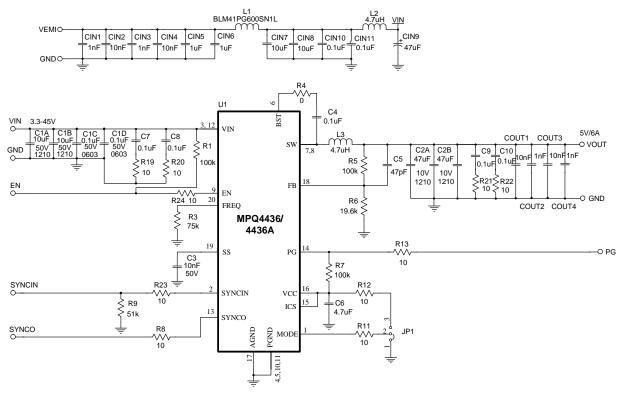


Figure 13: V<sub>OUT</sub> = 5V, f<sub>SW</sub> = 410kHz with EMI Filters



## TYPICAL APPLICATION (continued)

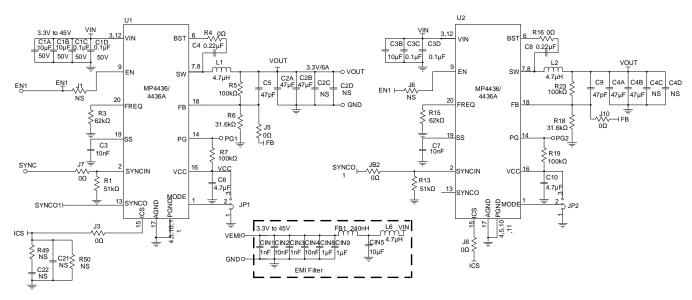


Figure 14: Dual-Phase,  $V_{OUT} = 3.3V$ ,  $f_{SW} = 470kHz$ 

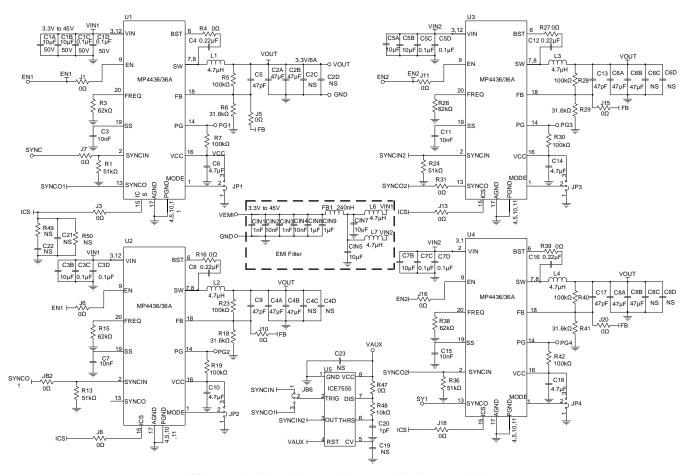
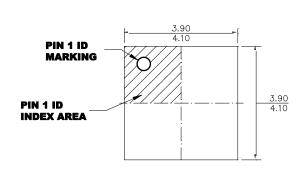
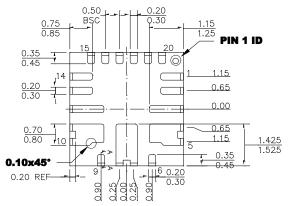


Figure 15: Four-Phase,  $V_{OUT} = 3.3V$ ,  $f_{SW} = 470kHz$ 

#### PACKAGE INFORMATION

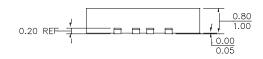
## QFN-20 (4mmx4mm) Wettable Flank

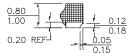




**TOP VIEW** 

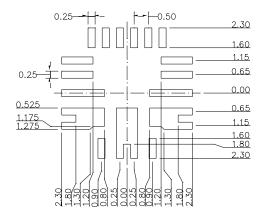
**BOTTOM VIEW** 





#### **SIDE VIEW**

**SECTION A-A** 



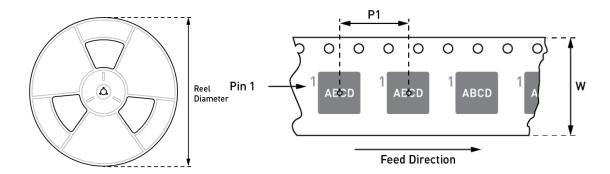
#### **NOTE:**

- 1) THE LEAD SIDE IS WETTABLE.
- 2) ALL DIMENSIONS ARE IN MILLIMETERS.
- 3) LEAD COPLANARITY SHALL BE 0.08 MILLIMETERS MAX.
- 4) JEDEC REFERENCE IS MO-220.
- 5) DRAWING IS NOT TO SCALE.

**RECOMMENDED LAND PATTERN** 



## **CARRIER INFORMATION**



Part Number	Package Description	Quantity/ Reel	Quantity/ Tube*	Reel Diameter	Carrier Tape Width	Carrier Tape Pitch
MPQ4436GRE-Z						
MPQ4436GRE-AEC1-Z	QFN-20					
MPQ4436AGRE-Z	(4mmx4mm)	5000	N/A	13in	12mm	-8mm
MPQ4436AGRE- AEC1-Z	(111111)					



## **REVISION HISTORY**

Revision #	<b>Revision Date</b>	Description	Pages Updated
1.0	6/25/2019	Initial Release	-
	Added "Automotive" in Applications section	1	
		Added the part number "MPQ4436AGRE"	3
		Added the description of "Connect a 51k $\Omega$ resistor between SYNCIN and GND" in SYNCIN pin function	1, 5
		Update recommended operating T <sub>J</sub> from 125°C to 150°C; tuned the format of the thermal resistance	6
		Updated the curves in Typical Characteristics section (the previous curve was wrong at 0°C caused by ATE test issue)	9–11
		Add the Case Thermal Rise curve at Vout = 5V	14
1.1	5/15/2020	Updated the efficiency curve's condition from 4.7µH to 3.3µH	1, 12–23
	0,10,2020	Update the load and line regulation test results	13–14
		Added the MSL Ratings, ESD Ratings, and Carrier Information sections	3, 6, 40
		Updated the ICS pin description to "Do not float this pin; connect it to VCC pin or VOUT that is at least 3V in a single-phase application"; updated the schematic and TAC layout figures accordingly	2, 5, 36, 37
		Updated the Operation section to say that SYNCIN should be applied after start-up is complete in AAM mode	32
		Added Figure 16 of the application circuit with EMI filter	37
		Removed information related to the fixed output version	1–4
1.2	11/08/2021	Updated Tape & Reel suffix from "–Z" to "-Z", added Tape & Reel suffix to part numbers in Carrier Information section	3, 37
1.2   11/08/2021		Formatting and grammar updates; updated the configurable switching frequency range from "350kHz to 530kHz" to "350kHz to 1000kHz"	All

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NCP81241MNTXG NTE7223 NTE7222 NTE7224 L6986FTR MPQ4481GU-AEC1-P MP8756GD-P MPQ2171GJ-P MPQ2171GJ-AEC1-P

NJW4153U2-A-TE2 MP2171GJ-P MP28160GC-Z MPM3509GQVE-AEC1-P XDPE132G5CG000XUMA1 LM60440AQRPKRQ1

LT8653SEV#PBF MP5461GC-P NCV896530MWATXG MPQ4409GQBE-AEC1-P S-19903DA-A8T1U7 S-19903CA-A6T8U7 S
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